

# RL78 Family

R01AN3795EU0100

Rev.1.00

## RL78 8-bit DAC Dithering

Aug 10, 2017

### Introduction

Some RL78 MCUs have a basic (unbuffered) 8-bit resolution Digital-to-Analog Convertor (DAC). This app note describes a method to increase the 8-bit DAC resolution to 12-bit effective resolution using a DAC amplitude dithering method.

### Target Device

RL78/G14 MCUs having 8-bit DAC and fSUB = 32768HZ oscillator. **Note:** Other RL78 MCUs having 8-bit DAC, 10-bit ADC, and DTC (Data Transfer Control), such as RL78/G11, G1F, F14, and F15 may also be used, but should be tested thoroughly to assure compatibility.

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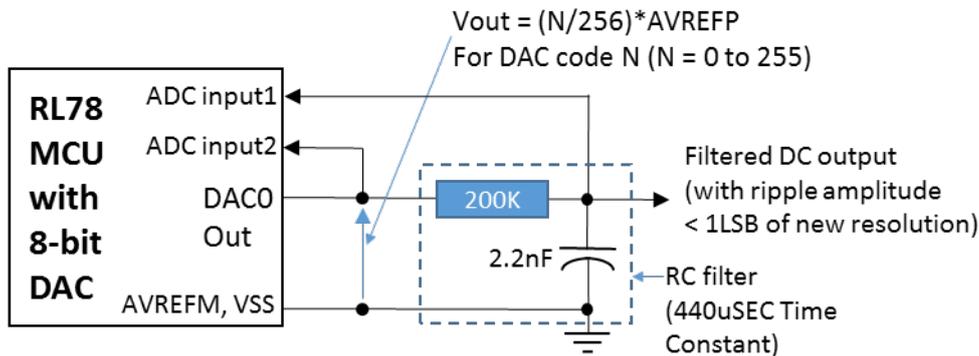
### 1. Overview

Typically MCUs having 10-bit or 12-bit DAC function are more expensive than those with 8-bit DAC. Therefore, it may be desirable to expand the 8-bit DAC resolution to achieve more than 256 possible DC voltage output levels. For example, in LED lighting or analog control systems that need a logarithmic type transfer function, a total of 256 linear levels may not be adequate, since the control needs to have finer resolution steps at lower drive levels. By modulating or dithering the DAC output between 2 consecutive 8-bit code output levels and smoothing the output by RC low-pass filter, a variable duty cycle can achieve more than 256 DC output levels from an 8-bit DAC.

This application note provides a framework to implement the DAC dithering method to increase the resolution of effective DAC output levels. It is up to the user to perform a full evaluation to measure DC accuracy, and response time versus DAC dithering update frequency and RC low-pass filter characteristics. The DC output accuracy and performance depends on the user's Hardware implementation, including measures to minimize residual noise level in their board design.

### 2. DAC Dithering method

The dithering method is accomplished by modulating the DAC output between 2 adjacent hex values in a periodic manner, automatically, by using DTC and ELC functions. For example, the simplest DAC dithering method could be toggling between a DAC output code of 0x80 (128 decimal) and 0x81 (129 decimal) with a 50%/50% ratio. This waveform would look like a square wave with a peak-to-peak value of 1 LSB out of 256 full-scale values available with 8-bit DAC output. If this square wave is filtered by a sufficiently designed low pass filter, an equivalent DC value of 128.5 out of full-scale 255 amplitude levels above 0Volts could be obtained, simulating approximately 9 bits of resolution. The low pass filter is used to reduce the dithering pattern ripple to less than 1 LSB at the new effective resolution. **Note:** Figure 1 example shows a 200KΩ series resistor and 2.2nF filter capacitor for reducing ripple in a repeating 320uSEC DAC dither pattern, but RC filter values could be modified as required if using different DAC dithering timing.

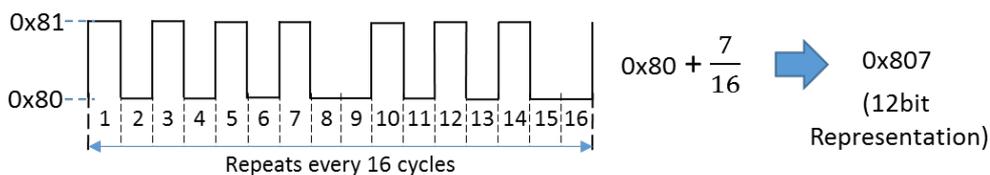


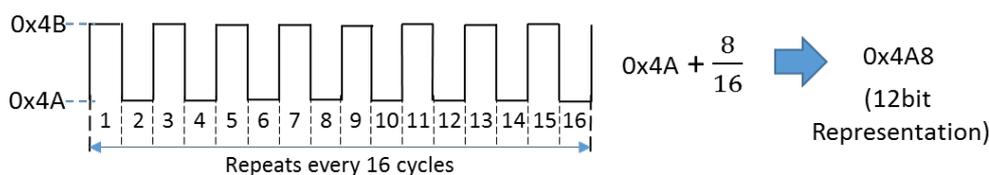
**Figure 1: Low Pass RC filtering of dither DAC Output**

#### 2.1 8-bit Dithering over 16 DAC output cycles

By modulating or dithering the DAC output values over a longer repeat period, with different dither patterns, more equivalent resolution bits can be obtained. This App note shows a method to create 4 additional bits of resolution, by outputting DAC output patterns that repeat every 16 cycles. With the 16 cycle pattern smoothed out by an RC low pass filter, it is capable of producing one of 15 intermediate DC voltage values between two consecutive 8-bit DAC values. Thus, the effective DC output resolution can be approximately 12 bits, with some limitations (described later).

(a) **Example 1: DAC output dithered between codes 0x80 and 0x81 (pattern for 7/16)**



(b) **Example 2: DAC output dithered between codes 0x4A and 0x4B (pattern for 8/16)**

The Data Transfer Control (DTC) and Event Link Controller (ELC) functions are used to automatically update the DAC output for 16 states of Dithering pattern, without CPU intervention needed until the last of 16 cycles, when the DTC is re-set for next 16-state operation. The RC filter with 440uSEC Time constant shown in Figure 1 is used to implement the DAC dithering Application Note Software project. With a DAC update cycle time of 20uSEC, and the dither pattern repeating every 320uSEC, a single stage RC filter with time constant of 440uSEC can reduce the ripple to less than 1LSB amplitude at the new, higher effective resolution, targeted at 12 bits. As shown in the **Figure 1** block diagram, the ADC input1 can be used to monitor the filtered DAC dithering, and apply a correction (closed-loop method) for better DC output accuracy, within the absolute accuracy of the ADC conversion measurements. By using the ADC Input2, the DAC output absolute errors before dithering can also be checked relative to the better 10-bit ADC accuracy. (see section 7.4)

## 2.2 DAC dithering control options:

### (a) Using open-loop DAC dithering WITHOUT ADC monitoring:

This method will create monotonic DC steps, with almost 12-bit resolution (limitations discussed later). However, the RL78 8-bit DAC has an overall error including DAC AINL (Analog Integral Non-Linearity) of +/-2.5 LSB out of 256 output values, which is close to +/-1% error relative to the full-scale analog range. Therefore the absolute value of the 12-bit effective (dithered DAC) uncompensated DC output may also have an error up to +/-2.5LSB relative to 8-bit resolution, and may not be linear over the full range of possible values. The open-loop method may be more useful when an absolute DC voltage level is not required, but DC level feedback is done by a human interacting with potentiometer adjustment or up-down pushbutton control. **Tradeoffs:** Using the open-loop DAC dither mode will settle to the target DC value more quickly (usually within 16mSEC) but will have larger absolute offset error compared to using the closed-loop method with ADC monitoring and feedback.

### (b) Using closed-loop DAC dithering WITH ADC monitoring and feedback:

The RL78 10-bit ADC maximum overall error is +/-3.5LSB (when using AVREFP and AVREFM full-scale analog voltage reference), which is slightly better than +/-1LSB error at the DAC 8-bit resolution. Therefore, it is possible to somewhat correct for both the intrinsic DAC +/-2.5 LSB max error and error from the DAC impedance loading. By calibrating the individual RL78 MCU ADCs on each board in the factory, even better accuracy might be obtained for the ADC conversion results, and therefore to the filtered DAC dithered DC output.

By summing and averaging 16 consecutive 10-bit ADC conversions, it is possible to measure the 12 bits effective resolution of the filtered DAC dithering DC output. The ADC measurement result is dependent on the ripple amplitude of the filtered DAC dithering output, and MCU/System noise riding on the PC board power, grounds and Analog reference voltage, which may not be truly random. Therefore, it's inevitable that each averaged/scaled sum of 16 consecutive 10-bit ADC conversion of filtered DAC dithered values will still vary by 1-2 LSB (or possibly more) out of 12-bit effective value. So there will be some random amplitude jitter on the corrected DAC dithered 12-bit effective resolution when using ADC averaged measurements and feedback.

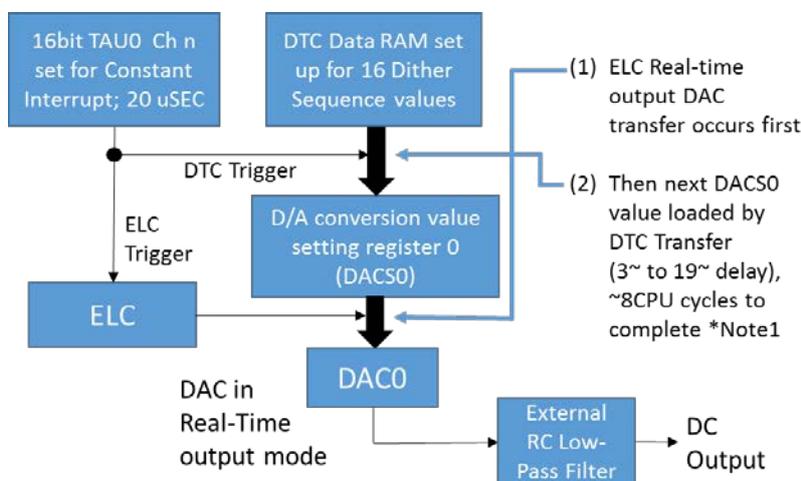
However, even with the amplitude jitter, the absolute DC output for 12-bit effective resolution can still correct for DAC output overall error, to the accuracy of the RL78's 10-bit ADC which is almost 3 times more accurate than the DAC. The app note Software project takes 256 ADC samples (16384HZ sample rate) and updates the Dither factor by +1, or -1 (for correction) or zero (if no offset is detected), every 256 ADC samples which is at a 64HZ (15.625mSEC) update rate. This simple correction method is often referred to as "bang-bang" feedback.

**Tradeoffs:** the closed-loop DAC Dithering method provides more DC accuracy, but takes longer (typically 32mSEC to 128mSEC) to settle to the target 12-bit effective DC value.

### 3. RL78 MCU resources used

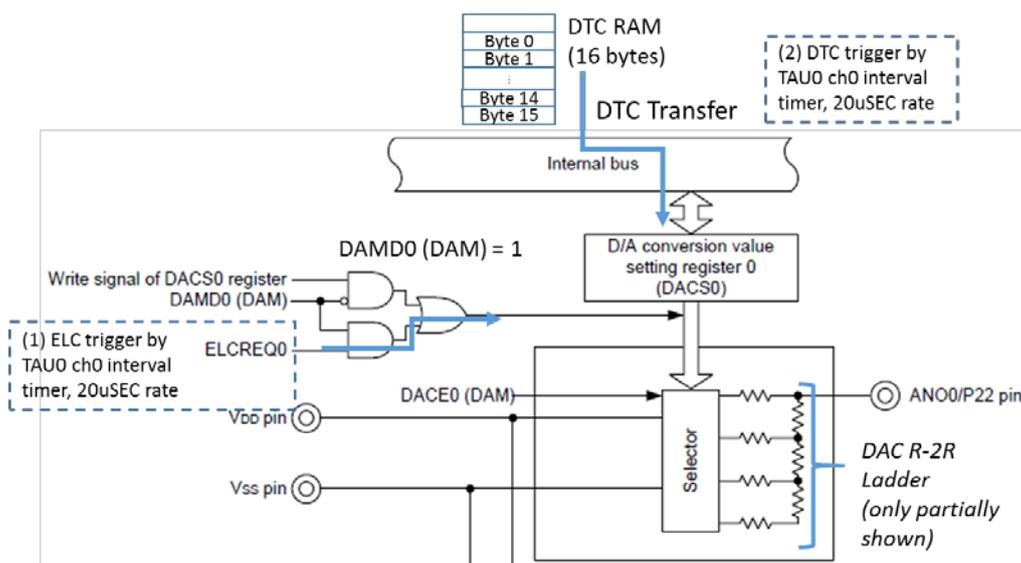
#### 3.1 MCU Hardware

- (1) 8-bit DAC
- (2) DTC (Data Transfer Control) operation to automatically load sequential 16 state dither pattern into DAC buffer DACS0. Takes about 8 CPU/System clock cycles per DTC transfer, with no CPU operation needed until after 16 DTC cycles to reset for next 16 DTC transfers.
- (3) ELC used to trigger DAC buffer contents to DAC output at a constant rate (20uSEC updates)
- (4) 16bit High speed timer TAU0 to create 20uSEC update rate, simultaneously triggering the next DAC buffer loading action, and the constant update to actual DAC output by ELC.
- (5) 10bit ADC conversions at 16384HZ rate (every 61 uSEC), using fSUB = 32768HZ clock with ADC Hardware Trigger wait mode from 12-bit Interval Timer
- (6) Optional UART1 output to capture live 12-bit averages of DAC dithering.



(\*Note1: After 16 DTC data transfers (320uSEC rate, DTC reset to repeat in TAU0 timer ISR)

**Figure 2: Automatic DAC Dithering using TAU0 timer, DTC, ELC and 8-bit DAC**



**Figure 3: DTC data transfers with ELC trigger to DAC Real-time output**

### 3.2 MCU CPU processing

Since the DAC output is being dithered, some CPU processing overhead is required:

- (1) DTC updates every 20uSEC; DTC uses 8 CPU cycles out of every 640 cycles when using 32MHZ CPU clock rate. The update rate could be adjusted for faster or slower updates if desired, as long as the RC low-pass filter time constant is adjusted accordingly.
- (2) DTC state reload (TAU0 channel0) interrupt every 16 DTC cycles, at 320uSEC rate.
- (3) 10-bit ADC conversion completion interrupt processing every 61 uSEC (16384HZ rate). 10-bit ADC conversions occur at 16384HZ rate using fSUB = 32768HZ clock in ADC Hardware trigger wait mode. However, the ADC HW triggered conversions themselves can operate in parallel with Software operation with no CPU intervention until ADC completion interrupt occurs. ADC conversions are an optional method to monitor RC low-pass filter output from DAC dithering pattern, and correct the DC value by modifying the dither pattern.
- (4) CPU processing the sum of 16 consecutive ADC conversion every 967.7uSEC (1024HZ rate)
- (5) Optional UART1 interrupts at 86.81uSEC per ASCII Character at 115.2Kbaud. This facilitates real-time monitoring of 16 consecutive averaged 10-bit ADC conversions of DAC dithering output, in a testing mode.

## 4. Software Environment

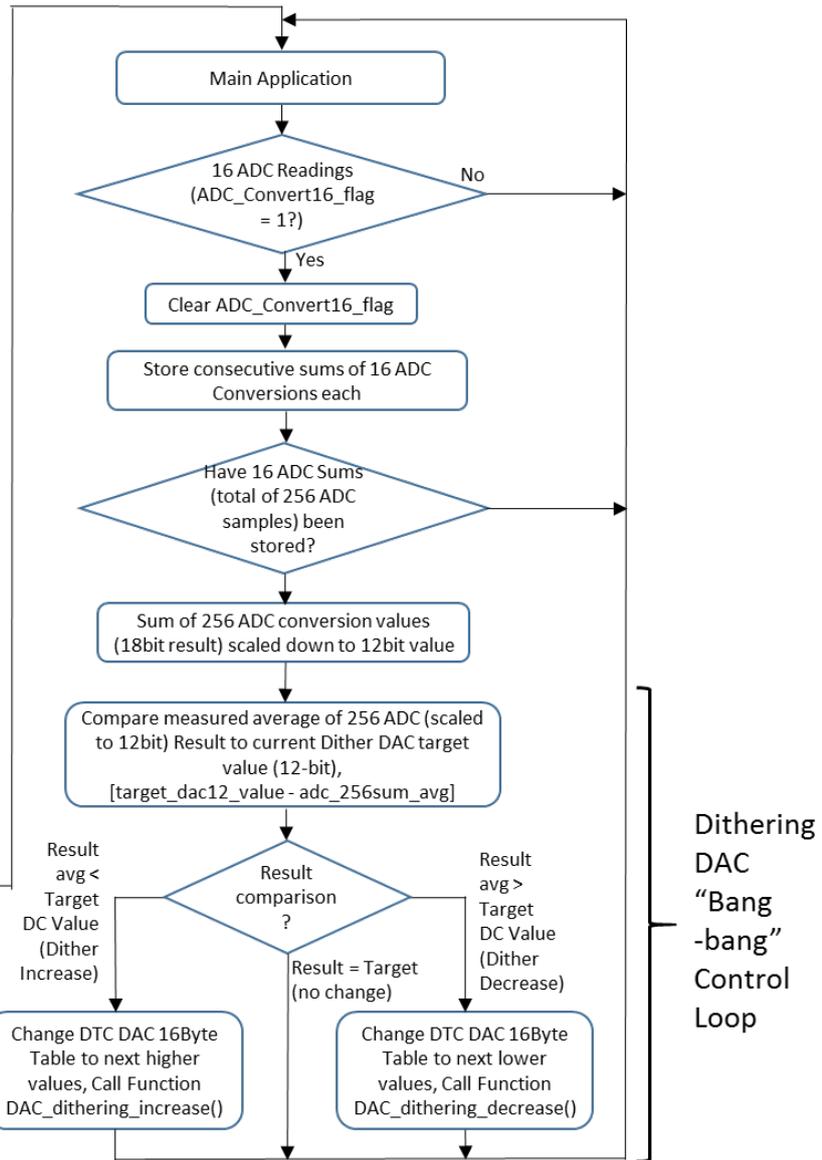
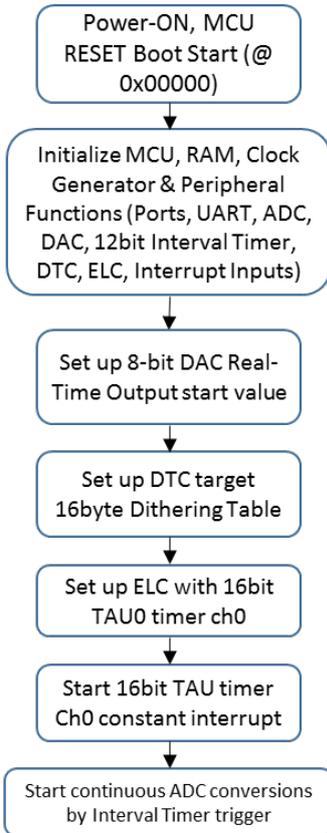
The sample Software project accompanying this application note uses the SW environment as follows:

IDE	RL78 Compiler	Compiler Version
Renesas e2studio v 5.2.1.010	CCRL	v1.04

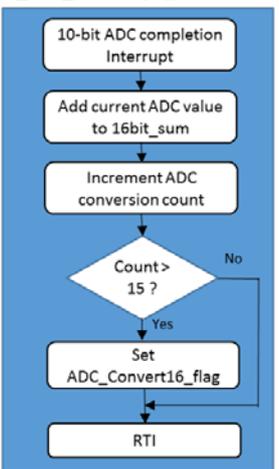
**Table 1: Sample Software project environment**

5. DAC Dithering (High-level Flowchart and Interrupt processing)

Start:

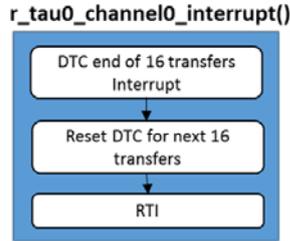


r\_cg\_adc\_user.c:  
r\_adc\_interrupt()



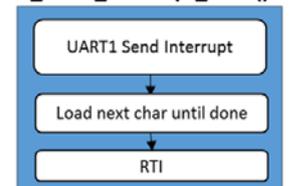
Constant ADC interrupt @16384HZ (61.04uSEC) HW trigger with Wait mode

r\_cg\_timer\_user.c:



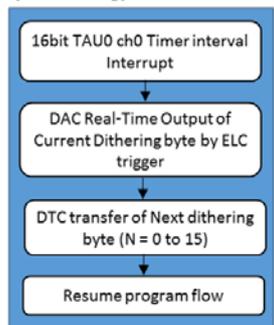
Constant 320uSEC Interrupt, end of 16 DTC transfers (TAU0 ch0 Interval Timer ISR)

r\_cg\_serial\_user.c:  
r\_uart1\_interrupt\_send()



86.81uSEC per ASCII Character at 115.2Kbaud.

(DTC/ELC hardware processing)



Constant 20uSEC Interrupt for DTC/ELC trigger (no ISR)

## 6. DAC dithering method details

### 6.1 DAC Dither Adder Sequence table

This DAC dither adder sequence table was designed to distribute the zeroes and ones pattern for highest repetition frequency, and thus minimize the ripple amplitude when filtered by a simple low pass RC filter. A zero means the base DAC value is used and a one means the base DAC + 1 value is used. Therefore, the Dither factor is the total duty cycle of N/16, where N = 0 to 15.

DTC State	Dither sequence (Dither factor)															
	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	0	1	1	1	1	1	1	1	1	0	0	0	0	0	0	0
2	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1
3	0	0	0	0	0	0	1	1	1	0	0	1	1	1	1	1
4	0	0	0	0	0	1	0	0	0	1	1	0	1	1	1	1
5	0	0	0	0	1	0	0	1	1	0	1	1	0	1	1	1
6	0	0	0	1	0	0	1	0	0	1	0	1	1	0	1	1
7	0	0	0	0	0	1	0	1	1	0	1	0	1	1	1	1
8	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1
9	0	0	1	0	1	0	1	0	1	1	0	1	0	1	0	1
10	0	0	0	0	0	1	0	1	0	0	1	0	1	1	1	1
11	0	0	0	1	0	0	1	0	1	1	0	1	1	0	1	1
12	0	0	0	0	0	0	0	1	0	0	1	1	1	1	1	1
13	0	0	0	0	1	1	0	0	1	1	1	0	0	1	1	1
14	0	0	0	0	0	0	1	1	0	0	0	1	1	1	1	1
15	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1
16	0	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1
DTC Dither sequence	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15

Base DAC value

Base DAC value + 1

**Table 2: Dithering adder sequence table**

Each vertical set of 16 adder values is for creating a new DTC sequence by adding to the base DAC value.

Examples:

- DTC Adder Sequence 0 has all zeroes (no dithering)
- DTC Adder Sequence 7 has 9 zeroes and 7 ones (7/16 dithering)
- DTC Adder Sequence 15 has one zero and 15 ones (15/16 dithering)

### 6.2 DTC Dithering adder example

**Example to create new DTC Dithering values:**  
 If base DAC value is 0x80, and adder is for 7/16 dithering (DTC Adder Sequence 7). Effective 12-bit target value = 0x807

DTC state	DAC Base Value		Dithering Adder Values		New DTC Sequence
1	0x80	+	1	=	0x81
2	0x80	+	0	=	0x80
3	0x80	+	1	=	0x81
4	0x80	+	0	=	0x80
5	0x80	+	1	=	0x81
6	0x80	+	0	=	0x80
7	0x80	+	1	=	0x81
8	0x80	+	0	=	0x80
9	0x80	+	0	=	0x80
10	0x80	+	1	=	0x81
11	0x80	+	0	=	0x80
12	0x80	+	1	=	0x81
13	0x80	+	0	=	0x80
14	0x80	+	1	=	0x81
15	0x80	+	0	=	0x80
16	0x80	+	0	=	0x80

**Table 3: Dithering adder example for target 12bit value 0x807**

### 6.3 Tradeoffs for DAC dither update rate versus CPU overhead

When implementing the DAC dithering method shown in this app note, it may be desirable to change the dithering rate, which may also require modifying the low-pass filter RC time constant. The tradeoff is that a slow dithering update rate, and longer RC filter time constant, will have a longer response time when changing the target DAC dithered 12-bit effective resolution value, especially when the target DC output value delta change is large. For example, changing from 10% to 90% of the DAC analog full scale reference (AVREFP-AVREFM) will take settling time that is proportional to the RC low pass filter time constant (approximately 2.5 to 3 RC time constants). However, a faster DAC dither rate will, on average, require more CPU/System clock cycles for DTC operation, ADC conversion complete interrupts and CPU processing overhead. Therefore, the user will need to determine a balance between optimum DC Slew rate performance and System/CPU processing time overhead.

### 6.4 Measuring DAC dithering ripple at RC low-pass filter output

The app note software project implements a 20uSEC DAC dither update rate that repeats every 16 periods (320uSEC total period) to create close to 12-bit effective resolution. The RC low pass filter should be designed to limit ripple to less than 1LSB at 12-bit effective resolution, which means less than 1/16 of the DAC dithering amplitude (DAC dithering is done at AVREFP/256 level, with 1LSB peak-to-peak amplitude), and probably closer to 1/2 LSB at 12-bit effective resolution (1/32 of AVREFP/256, 1LSB amplitude). This app note sample project uses 200K series resistor and 2.2nF capacitor for a 440uSEC RC time constant. Using the 440uSEC RC time constant achieves about 0.69 LSB typical ripple (relative to 12-bit effective resolution) when the dither sequence is 7/16, which is worst case. The best case is about 0.36 LSB typical ripple (relative to 12-bit effective resolution) when the dither sequence is 8/16.

It is difficult to measure the dithering ripple amplitude after RC filtering for these reasons:

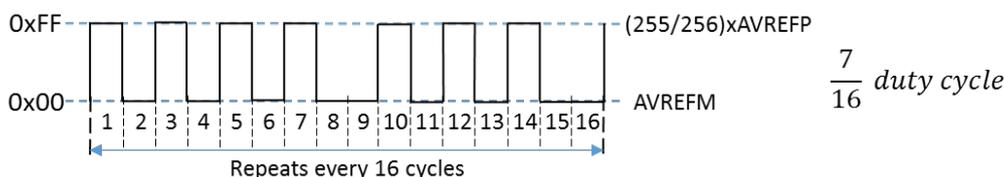
- (1) The ripple amplitude for 12bit effective DAC resolution is typically less than 0.75mV-1.25mV depending on VDD value. In Table 2 example below, VDD values of 3.072Volts and 5.12 Volts (similar to typical 3Volt and 5Volt power supplies) are shown to make the steps easy to represent. At these 0.75-1.25millivolts levels (or less) the System/MCU noise levels may be as high the DAC dithering ripple value.

	DAC/ ADC Reso- lution	Each LSB step, when VDD =	
		3.072 Volts	5.12 Volts
Using RL78:			
DAC	8bit	12 mV	20 mV
ADC	10bit	3 mV	5 mV
DAC dithering	12bit	0.75 mV	1.25 mV

**Table 4: DAC/ADC resolutions**

- (2) Additionally, the high output impedance of the 8-bit DAC (5K-39KΩ) and example 200KΩ series resistance of RC low pass filter would seem to require using a standard X10 (10MΩ input impedance) oscilloscope probe, since a 1MΩ probe would load down a 200K source impedance significantly. However, the actual ripple amplitude into the scope input after a X10 probe 10:1 voltage reduction will typically be too low (possibly less than 100microvolts pk-pk), and unreadable on most standard oscilloscopes.
- (3) As an alternative, if a 1MΩ scope probe is used, then the probe impedance significantly loads down the RC low-pass filter output amplitude, almost 17% when using series R of 200K. Also, since the RC filtering reduces the DAC dithered ripple amplitude to less than 1LSB at 12bits effective resolution, the digital sampling of the storage scope will have problems capturing the ripple waveform accurately, since most digital scopes typically sample with 10-bit resolution for analog signals.

The easiest way to measure relative DAC dither ripple amplitude at the RC low-pass filter output is to use maximum DAC output amplitude of 0x00 to 0xFF peak-peak pulsing and measure with a X10 (10MΩ input impedance) scope probe. The ripple amplitude reduction of the RC filter output fed with full 0volt to (255/256)\*AVREFP pk-pk voltage swings will be the same as 1LSB (relative to 8-bit resolution) pulse waveform attenuation on the RC filter output. Then, the filtered DAC dithering waveform is larger by a factor of 255 and the resulting filtered ripple amplitude is approximately 60mV-100mV pk-pk (or greater, depending on AVREFP, VDD) and much easier to measure. A dither pattern of 7/16 in Figure 4 is the same as 7/16 duty cycle.



**Figure 4: Method to measure RC low-pass filter output ripple**

This method is included in the Application note Software Project as a test mode to facilitate Dithering ripple amplitude measurement. (when `dac_dither_full_mag_test_flag = 1;` in `r_main.c`)

### 6.5 Typical DAC dithering ripple amplitude from RC low filter

Using the section 6.4 ripple measuring method, the following tables shows approximate measured RC low pass ripple amplitudes for each of the 15 possible dithering patterns. This table was generated from empirical data, using a 320uSEC repeating period DAC dithering pattern and RC low-pass filter with time constant = 440uSEC. If the User desires to implement a different DAC dithering repeat period and change the RC low-pass filter time constant, it may be useful to re-measure the RC filter output ripple to confirm filter performance.

From a frequency domain standpoint, in Table 5 it can be seen the largest ripple amplitude is for the lowest Dither pattern repeat frequency of 16 cycles, and has the lowest ripple amplitude at the highest Dither pattern repeat frequency of 2 cycles. That is because the RC low-pass filter attenuates increasingly higher frequencies more.

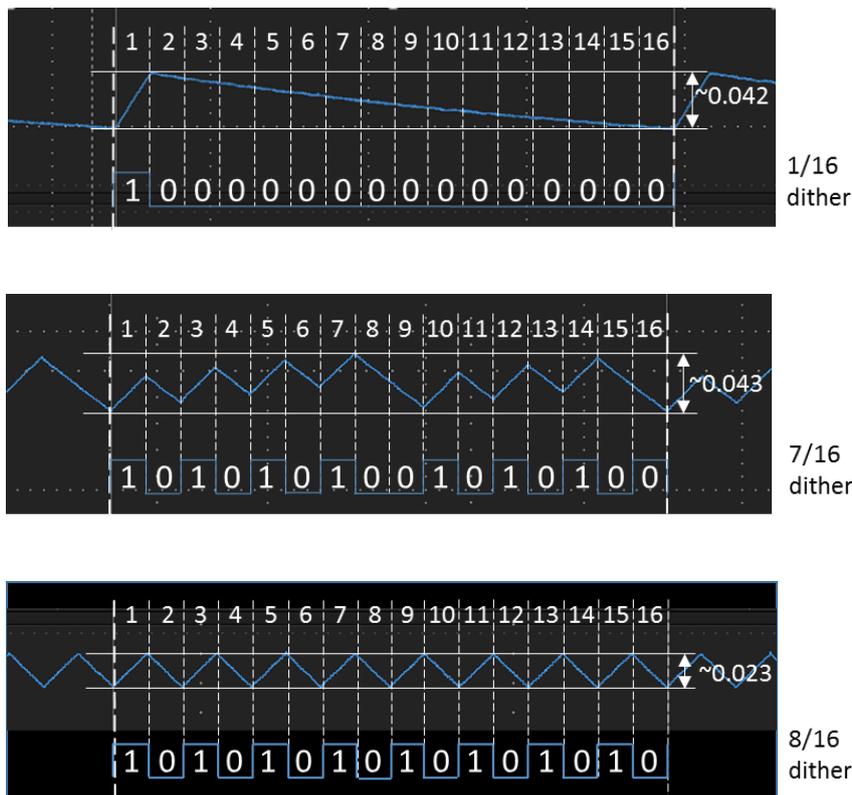
Dither Sequence Number N (duty = N/16)	Dither Sequence Pattern repeats every N cycles of DTC transfer	Ripple Amplitude relative to 1LSB of 8bit DAC	Ripple Percentage of 1LSB at 12bit effective resolution
1, 15	16	0.0416	67%
2, 14	8	0.0387	62%
3, 13	16	0.0420	67%
4, 12	4	0.0337	54%
5, 11	16	0.0422	68%
6, 10	8	0.0389	62%
7, 9	16	0.0434	69%
8	2	0.0227	36%

**Table 5: Relative ripple amplitude**

(based on 320uSEC dither repeat period, 440uSEC RC low-pass filter time constant)

The ripple amplitude listed in Table 5 is the fraction relative to two adjacent DAC codes peak-peak amplitude (example; 0x80 and 0x81) normalized to a value of one. When this is extrapolated to a 1LSB pk-pk amplitude of 8-bit DAC, the ripple percentage becomes approximately 36%-69% of 1LSB at 12-bit resolution.

As can be seen in Table 5, the minimum ripple is for Dithering sequence N = 8, where the DAC output looks like a square wave between 2 adjacent DAC values (example: 0x80 and 0x81). The worst case ripple amplitude occurs for dither sequence N = 7 and N = 9, where the ripple amplitude is almost twice that of N = 8. It should be noted that the ripple amplitude is identical for Dither sequence N and 16-N, where N = 1 to 15. For example, the ripple amplitude for Dither sequences 3 and 13 is the same, and for Dither sequences 7 and 9 is the same. That is because the Dither Sequence pattern is just inverted between sequence 3 and 13, and between sequence 7 and 9, and therefore the ripple magnitude is the same amplitude but inverted for inverted dither pattern sequences.

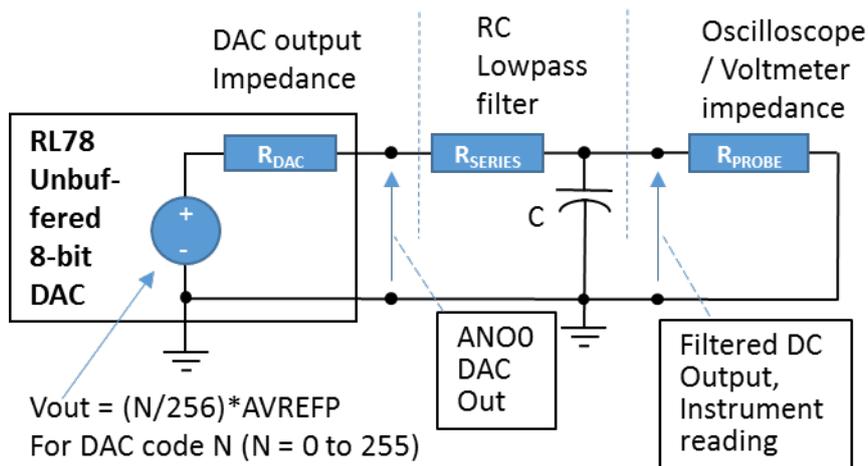


**Figure 5: Typical RC low-pass filter ripple waveforms**  
(ripple output listed as a fraction of input normalized to 1.0)

### 6.6 Understanding RC low pass filter output loading

This app note sample project uses a 200KΩ series resistance and C = 2.2nF RC filter to avoid loading the unbuffered 8-bit DAC too much. There is a tradeoff on RC filter impedance. If the RC filter series resistance is too low, approaching the typical output DAC impedance, R = 5K-10KΩ, then there will be a large voltage drop due to loading the unbuffered DAC output too much. The DAC output impedance R is not specified in RL78 MCU electrical specifications section, but is estimated to be 5K-10KΩ typically, and possibly as high as 39KΩ worst case.

However, if the series R of the RC filter is too large, then there will be larger measurement errors when using a 10MΩ input impedance of a typical scope probe or DC voltmeter (10MΩ to 11MΩ typical for instrumentation quality voltmeter). Also, as impedance of the RC filter goes higher, the external system noise may affect the desired DAC-like 12-bit effective DC output value more. For example, an R = 200KΩ and C = 2.2nF gives a 440uSEC time constant compared to R = 2MΩ and C = 220pF where the RC time constant is still 440uSEC, but the filter impedance is 10x higher for the latter values.



**Figure 6: Impedance Model of DAC output with RC Low-pass filter and instrument loading**

In **Figure 6** (Impedance model) above, loading both the ANO0 DAC output and RC Low-pass filter output with x10 (10MΩ) scope probe or 10MΩ input voltmeter will affect the results somewhat. The total DAC load will still be greater than 5MΩ (10MΩ in parallel with 10.2MΩ), greater than the RL78 minimum 8-bit DAC loading resistance of 4MΩ minimum for guaranteed specification of DAC overall error = +/-2.5% maximum.

However, if using a X1 (1MΩ) scope probe on either the ANO0 DAC output or the (filtered) RC Low-pass filter DC output, there will be significant errors. For example, if a 1MΩ Scope probe is placed only on the RC low pass filter output (no dithering, with R<sub>DAC</sub> = 10KΩ and R<sub>SERIES</sub> = 200KΩ), the output will result in approximately:

$$\begin{aligned}
 RC \text{ filtered output} &= R_{\text{PROBE}} / (R_{\text{DAC}} + R_{\text{SERIES}} + R_{\text{PROBE}}) * \left(\frac{N}{256}\right) * AVREFP \\
 &= 1\text{M}\Omega / (0.01\text{M}\Omega + 0.2\text{M}\Omega + 1\text{M}\Omega) * \left(\frac{N}{256}\right) * AVREFP \\
 &= 0.826 * \left(\frac{N}{256}\right) * AVREFP
 \end{aligned}$$

**Conclusion:** Using a 1MΩ oscilloscope probe or voltmeter impedance on RC filter output will reduce the DC level by (100% - 82.6%) = ~17.4%

Alternatively, if a 10MΩ probe is used:

$$\begin{aligned}
 RC \text{ filtered output} &= 10\text{M}\Omega / (0.01\text{M}\Omega + 0.2\text{M}\Omega + 10\text{M}\Omega) * \left(\frac{N}{256}\right) * AVREFP \\
 &= 0.979 * \left(\frac{N}{256}\right) * AVREFP
 \end{aligned}$$

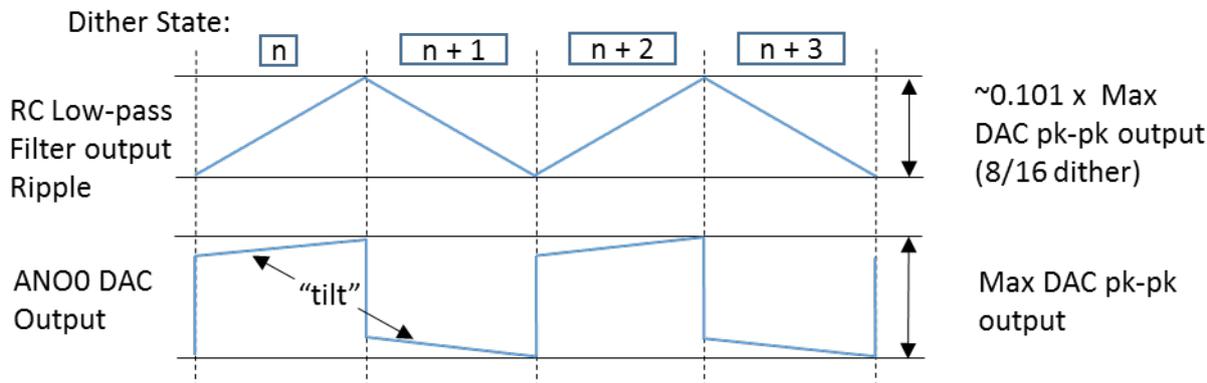
**Conclusion:** Using a 10MΩ oscilloscope probe or voltmeter impedance on RC filter output will reduce the DC level by (100% - 97.9%) = ~2.1%. The RL78 specification for minimum resistance 8-bit DAC loading is 4MΩ, to meet the max Overall 8-bit DAC error of +/-2.5LSB but there can still be up to -2.1% level drop between no loading and 10MΩ DC loading.

In actuality, almost any DC loading will lower the RC filtered DC output by some percentage. The closed loop correction mode can somewhat help overcome the DC loading drop by increasing the DAC dither level but cannot compensate for all loads at higher 12-bit effective codes. The open loop DAC dithering method will definitely exhibit lowered DC output at the RC filter when loading resistance is decreased (smaller R value). In empirical tests, even a 10MΩ load on the combination R= 200KΩ and C = 2.2nF, RC filter caused the filter output ADC reading to droop to 0xF9F code reading when the Target DC value was set to 0xFE F. However, setting the Target DC value to 0xF9F, the closed loop method as able to compensate to an actual average of 0xF9F. (typical example, not worst case.) The ADC input impedance is extremely high (maybe >100MΩ) and typically won't affect the RC filter loading for R = 200KΩ.

The result is that almost any normal test instruments with 10MΩ input impedance will adversely affect the DAC dithering results relative to a very high (50MΩ-100MΩ) impedance buffer amplifier or MCU ADC input.

### 6.7 DAC Dithering output vs ripple output observations

If 10MΩ scope probes are attached to both the ANO0 DAC output and the RC filter output, the observed waveforms will be approximately as shown in **Figure 7**.



**Figure 7: Example of measuring RC Low-pass filter output at max DAC pk-pk amplitude**

**Notes:**

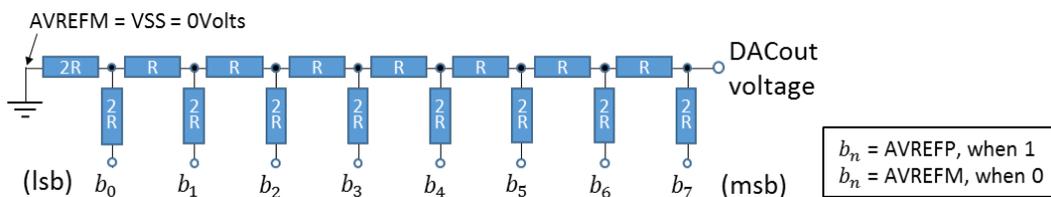
- Figure 7. Waveforms not to scale, and "tilt" amplitude is exaggerated to show effect
- Max DAC pk-pk output is for 0x00 to 0xFF amplitude =  $(255/256) \times (AVREFP - AVREFM)$ , although the actual amplitude will be reduced by about 2.1% due to 10Megohm scope probe loading

The "tilt" on ANO0 DAC output (slightly exaggerated here) is normal due to the internal DAC output impedance 5KΩ-10KΩ, acting as a voltage divider with the 200KΩ RC filter series resistor, and the tilt shows up as the RC filter capacitor is charging and discharging. When AVREFP = VDD = 5Volts, a DAC output impedance of 5KΩ-10KΩ can cause a tilt "difference" value of approximately 61millivolts (with 5KΩ DAC impedance) to 119millivolts (with 10KΩ DAC impedance) and could theoretically be higher if DAC output impedance ( $R_{DAC}$ ) = 39KΩ worst case.

If RC filter output ripple measurements are made, either the  $AVREFP \times (255/256)$  value can be used as a reference approximation, or the max DAC peak to peak amplitude seen on ANO0 DAC output can be used.

## 7. Attributes of D/A Convertors (DAC) using R-2R ladder

### 7.1 R-2R resistor ladder used in RL78 8-bit DAC



**Figure 8: R-2R ladder configuration**

On a D/A convertor R-2R resistor ladder, the output impedance is R. The RL78 DAC is unbuffered, meaning that if R is in the range of 5KΩ to 39KΩ, any significant loading can cause the output to "droop", causing a DC error. In fact the RL78 electrical specification for 8-bit DAC shows a minimum loading resistance of 4MΩ to still meet the worst case DAC output voltage of +/-2.5 LSB maximum overall error.

### 7.2 Ideal equation for 8-bit DAC output voltage

Using the RL78 full scale Analog reference voltages of AVREFP and AVREFM minimizes noise coupling for both the DAC and ADC units, and gives the optimum accuracy for 10-bit ADC conversion (+/-3.5LSB max overall error). So it is recommended to use the AVREFP/AVREFM voltage reference for the DAC dither project. Then, for the 8-bit DAC, there are 256 possible voltage outputs, but only 255 steps above the 0x00 DAC output value. Since the full-scale

Analog reference value is AVREFP-AVREFM, but maximum code is 0xFF (255 decimal), the maximum DAC output is  $255/256 \cdot AVREFP$  (when AVREFM = 0Volts). This can be seen in the following equations (assuming no loading on the unbuffered DAC output) in the ideal case with no other DAC output errors:

$$DAC_{out} \text{ voltage} = \left( \frac{b_7}{2} + \frac{b_6}{4} + \frac{b_5}{8} + \frac{b_4}{16} + \frac{b_3}{32} + \frac{b_2}{64} + \frac{b_1}{128} + \frac{b_0}{256} \right) \cdot (AVREFP - AVREFM)$$

When AVREFM = VSS = 0Volts, and DAC code is 0xFF;

$$DAC_{out} \text{ voltage} = \left( \frac{1}{2} + \frac{1}{4} + \frac{1}{8} + \frac{1}{16} + \frac{1}{32} + \frac{1}{64} + \frac{1}{128} + \frac{1}{256} \right) \cdot AVREFP = \frac{255}{256} AVREFP$$

Actually this is the case for all DACs (and successive approximation type ADCs) that use the R-2R resistor ladders, that the maximum DAC output voltage (or maximum ADC input voltage) is always 1 LSB below the full-scale analog voltage, assuming the ideal case with no other errors but in reality there are DAC errors due to slight AVREFP and AVREFM voltage differences from one 2R tap to another, as well as minute differences in actual R resistance values!

Range	ratio of AVREFP	8bit DAC Output Code		10bit ADC conversion code		ratio of AVREFP	Range	
		Hex value	Decimal	Hex value	Decimal			
Not Valid	256/256	0x100	256	0x1000	1024	1024/1024	Not Valid	
				0x3FF	1023	1023/1024		
				0x3FE	1022	1022/1024		
				3FD	1021	1021/1024		
Valid Range	255/256	0xFF	255	0x3FC	1020	1020/1024	Valid Range	
				0x3FB	1019	1019/1024		
				0x3FA	1018	1018/1024		
				0x3F9	1017	1017/1024		
	254/256	0xFE	254	0x3F8	1016	1016/1024		
				0x3F7	1015	1015/1024		
				0x3F6	1014	1014/1024		
				0x3F5	1013	1013/1024		
	.	.	.	.	.	.		.
	.	.	.	.	.	.		.
	.	.	.	.	.	.		.
	1/256	0x01	1	0x007	7	7/1024		
0x006				6	6/1024			
0x005				5	5/1024			
0x004				4	4/1024			
0/256	0x00	0	0x003	3	3/1024			
			0x00	2	2/1024			
			0x00	1	1/1024			
			0x00	0	0/1024			

**Table 6: Ideal DAC/ADC max values as ratio of AVREFP**

(ideal values, not including real-world DAC and ADC accuracy errors)

### 7.3 Limitation of Dynamic range using DAC Dithering method

There are 256 possible output values of the 8-bit DAC, but the dithering requires toggling between 2 adjacent DAC output values. Using a 16 state dithering sequence there are only 15 different dithering sequences between any 2 DAC output states. As can be seen, the Dither adder sequence 0 (in Table 2.) is all zeroes which means no dithering is done.

Otherwise, dithering can only be applied on 255 combinations of 2 adjacent DAC codes, so there are only 4081 possible values:

$$\begin{aligned}
 \text{Maximum range of Dithered "12-bit" output values} &= \\
 &= 256 \text{ (DAC codes 0x00 to 0xFF, no dithering)} + 255 \times 15 \text{ dithering sequences} \\
 &= 4081 \text{ values,} \\
 &= \underline{0-4080 \text{ decimal (0x000 to 0xFF0)}}
 \end{aligned}$$

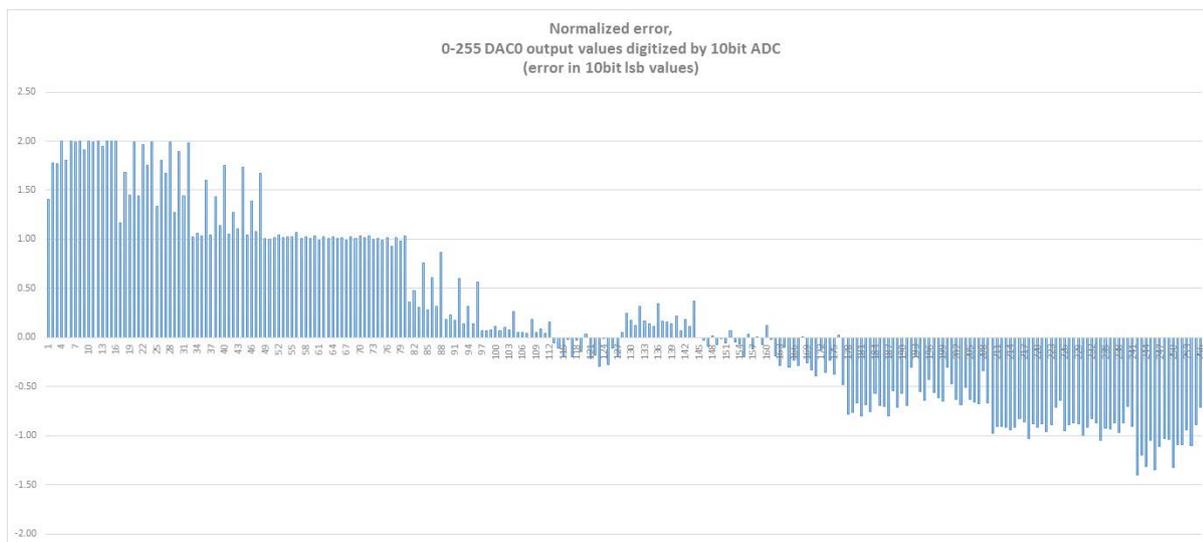
So when using the DAC Dithering method, the effective 12-bit resolution target setting cannot exceed the 12-bit code of 0xFF0, which is the same maximum of the 8-bit DAC output code.

**Note:** Although the DAC dithering output setting is limited to a max target value of 0xFF0, it is possible that ADC conversion values of 0xFF1 to 0xFFF may still occur, due to DC offsets/errors in both the DAC output and ADC conversion.

### 7.4 RL78 8-bit DAC accuracy relative to 10-bit ADC accuracy

The RL78 8-bit DAC electrical specification only specifies one error value; Overall error of +2.5LSB max (for 4MΩ loading or greater), which includes AINL (Analog Integral Non-Linearity) error. In reality, the DAC Overall error includes Zero-scale, Full-scale and Differential Non-Linearity (DNL) error. What this means is the 8-bit DAC output absolute error can change somewhat from one DAC code to another, throughout the range of the DAC output code values. The +/-2.5LSB max error for 8-bit DAC is equivalent to +/-10LSB variance range for 10bit ADC conversions. Since the RL78 10-bit ADC overall error is +/-3.5LSB max (when using ADC full-scale analog reference of AVREFP and AVREFM connections), the 10-bit ADC has almost 2.9X better accuracy than the 8-bit DAC output accuracy. However, the 10-bit ADC accuracy of +/-3.5LSB (at 10-bit resolution) overall error means that the overall error in monitoring the 12bit effective Dithered DAC (RC filtered) output average value could be +/-14LSB (4x 3.5) or more relative to the ideal 12bit equivalent, effective DC value from DAC dithering.

As can be seen in this graph (Figure 9.), 8-bit DAC output varies from code-to-code when measured by averaged 10-bit ADC conversions. This graph shows a general trend for the DAC output to be high (> +1LSB at 10bit resolution) for codes of 0 to 48 decimal, and to be low (< -1LSB at 10bit ADC resolution) for output codes of about 242 decimal and higher. This graph is just measured on one RL78/G14 MCU, and may not represent a typical RL78/G14 MCU. On one hand, this data seems to indicate the 8-bit DAC output accuracy can be tighter than the DAC Overall error maximum specification, but still has an error range of +2LSB to -1.5LSB at 10-bit ADC resolution. However, this graph does not address the possible inherent 10bit ADC conversion error of +/-3.5LSB (10bit resolution).



**Figure 9: Typical 8-bit DAC output measured by 10-bit ADC**  
(each point averaged from 256 consecutive ADC conversions per DAC code)

## 8. Typical monitoring results of DAC dithering Output

The app note Software Project includes an optional UART1 output (provided on RSKRL78G14 board DB-9 connector) to provide real-time monitoring of the DAC dithering output, both before and after RC filtering. UART1 is set for 115.2Kbps, and each 10bit character takes about 86.8uSEC. Each hex value of 3 ASCII characters (plus comma or LF character) in section 8.1 and 8.2 is output at 1024HZ (976.6uSEC) rate and takes about 347uSEC for 4characters. The UART1 print function was intended for troubleshooting and accuracy measurement, but is not needed to implement the DAC dithering open-loop or closed-loop functions.

## 8.1 UART output for RC filtered DAC dithering, open-loop mode

When variables `enable_print = 1` and `g_closed_loop = 0` in `r_main.c`, UART1 will output the sum of 16 consecutive ADC conversion, scaled down to a 12bit Hex value, with no correction on the DAC dithering. The first (single) hex value is the target 12-bit effective dithered DAC DC value. Each line thereafter represents 16 averaged/scaled RC filtered output values (each value is sum of 16 ADC 10-bit conversions). So each line occurs at 64HZ rate (16384HZ sample rate/256 total samples). In this example output, the `target_dac12_value = 0xFE6`. After about 16mSEC startup time, the dithered DAC RC filtered output settles to `0xFE2`, which is an offset of about -4 steps below the target `0xFE6` value in 12bit effective DAC resolution.

```
FE6
FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF
FFF,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2
FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2,FE2
(...continues indefinitely)
```

**Figure 10.: UART1 print monitoring in Open-loop mode**

## 8.2 UART output for RC filtered DAC dithering, closed-loop mode

When variables `enable_print = 1` and `g_closed_loop = 1` in `r_main.c`, UART1 will output the sum of 16 consecutive ADC conversion, scaled down to a 12bit Hex value, with the DAC Dithering value corrected once on each line (15.625mSEC correction rate). The data output is the same format as described in section 8.1 above. In this example, again the `target_dac12_value = 0xFE6`. However due to the closed-loop ADC measurement and correction, the dithered DAC RC filtered output settles to the target `0xFE6` value in 12bit effective DAC resolution but takes about 7 periods of 15.625mSEC correction to achieve stable output.

```
FE6
FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF,FFF
FFF,FE2,FE2,FE2,FE3,FE2,FE2,FE2,FE2,FE3,FE2,FE2,FE2,FE2,FE3,FE2
FE2,FE2,FE2,FE2,FE2,FE2,FE3,FE3,FE3,FE3,FE3,FE3,FE3,FE3,FE3,FE3
FE3,FE3,FE3,FE3,FE3,FE3,FE3,FE4,FE4,FE4,FE4,FE4,FE4,FE4,FE4,FE4
FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5,FE5
FE5,FE5,FE5,FE5,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6
FE6,FE6,FE7,FE7,FE6,FE7,FE6,FE7,FE7,FE7,FE7,FE7,FE7,FE7,FE7,FE7
FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6,FE6
(...continues indefinitely)
```

**Figure 11.: UART1 print monitoring in Closed-loop mode**

## 8.3 UART output for measuring DAC output offset errors

When `g_dacout_test_flag = 1` in `r_main.c`, and function `dacout_test_to_adc_input()` is run, the 10bit ADC measures each of 8-bit DAC codes `0x00` to `0xFF`, for 256 conversions per DAC output code. Each line evaluates a single 8-bit DAC output code, starting with `0x00` and ending with `0xFF`. Each 4 character value corresponds to the sum of 16 consecutive 10-bit ADC conversions, so each value can contain up to 14bit results, not scaled down. Possible output range is `0x0000` to `0x3FFC` max (0 to 16380 decimal).

From this example below, it is seen the 8-bit DAC code of `0xFF`, when measured 256 times has a 14bit average value of `0x3FB0`, or about `0x3FB` at 10-bit resolution, which is about 1LSB (at 10-bit resolution) below the predicted max value for `0xFF` DAC output with 10-bit ADC conversion. (Reference Table 6.)

```
0013,0015,0015,0012,0013,0012,0013,0010,0013,0010,0012,0012,0012,0013,0012,0013
005E,005D,005C,005D,005B,005A,005C,005D,005A,005E,005B,005D,005D,005B,005D,005B
0099,009B,0099,009B,0097,009A,009A,009C,009B,009B,009A,0097,009D,0099,0098,009B
⋮
3EF0,3EF0,3EF0,3EEE,3EEE,3EF1,3EEE,3EEE,3EF0,3EF0,3EF7,3EF1,3EEC,3EF0,3EF0,3EF0
3F2A,3F2E,3F2D,3F2E,3F2A,3F2E,3F35,3F2F,3F37,3F2B,3F35,3F2B,3F2E,3F2D,3F2E,3F2F
3F6A,3F70,3F70,3F70,3F70,3F70,3F70,3F70,3F6F,3F71,3F70,3F70,3F70,3F70,3F70
3FB0,3FAF,3FAF,3FB6,3FB1,3FB5,3FB0,3FB2,3FAF,3FB4,3FB0,3FB0,3FB1,3FB0,3FB0,3FB0
(completes after 256 total lines)
```

**Figure 12.: UART1 print monitoring for all 256 DAC codes out to ADC input**

The Figure 9. Plot in section 7.4 was generated from `dacout_test_to_adc_input()` UART1 data output similar to the above data in Figure 12, averaged and scaled down to 10bit equivalent resolution.

## 9. DAC Dithering increase/decrease, closed-loop algorithm

In the DAC Dithering close-loop mode, the sum of the last 256 ADC conversions (10bits x 256 = 18bit result) is scaled down and rounded off to a 12bit effective result every 15.625mSEC. Then the 12bit actual (averaged) result is compared to the User settable 12-bit `target_dac12_value`. If target and measured values are equal, then no DAC dithering correction is made. If the actual measured value is less than the target value, the dithering factor is increased by one bit value in 12-bit resolution. If the actual measured value is greater than the target value, the dithering factor is decreased by one bit value (12-bit resolution).

Care is taken not to produce a Dithering base value and factor that is out of range. Depending on the previous DAC output Base Value, either the Base Value, the Dithering factor, or both values will need to be updated into the 16byte RAM table transferred to DAC by DTC data transfers.

### 9.1 DAC Dithering Increase

For Dithering increases, a special case occurs when the previous DAC Dithering value is `0xFF0`, and no increase is possible, since Dithering can only occur between DAC output codes `0xFE` and `0xFF` to produce 12bit DAC effective codes of `0xFE0` to `0xFEF`. A constant DAC output code of `0xFF` represents `0xFF0` in 12-bit resolution and no further increase is possible. Of course, there is typically some lowered DC offset when DAC output is `0xFF` code and the 12bit effective DAC value is slightly less than `0xFF0`.

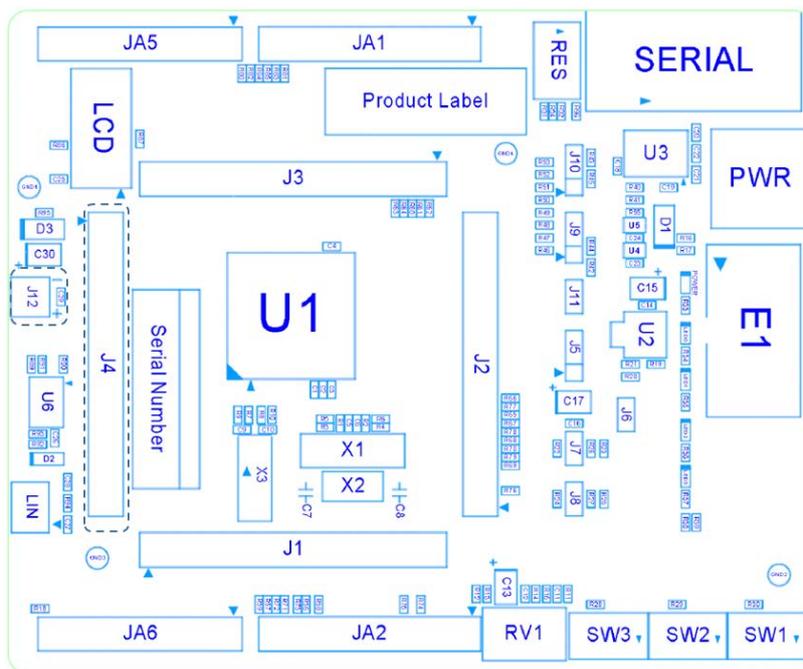
### 9.2 DAC Dithering Decrease

For Dithering decreases, a limit case occurs when the previous DAC Dithering value is `0x000`, and no decrease is possible, since Dithering can only occur between DAC output codes `0x00` and `0x01` to produce 12bit DAC effective codes of `0x000` to `0x00F`. A constant PWM output code of `0x00` represents `0x000` in 12-bit resolution and no further decrease is possible.

## 10. HW implementation for Sample SW project

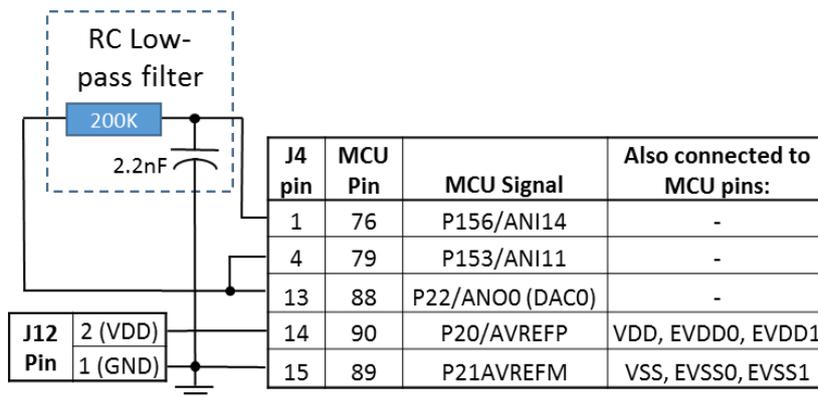
The application note Sample SW project was developed on an RSKRL78G14 board, populated with 100pin RL78/G14 (device R5F104PJ). This board layout was designed to maximize access to all the MCU pins, and provide a preliminary prototyping platform for customer RL78/G14 designs. However, the printed circuit board layout may not be optimum for lowest Analog noise riding on the RL78 power supply and ground lines. Nevertheless, the 10-bit ADC specification show the lowest overall ADC conversion errors ( $\pm 3.5\text{LSB}$  at 10-bit resolution) when the AVREFP and AVREFM lines are used to provide the Full-scale analog voltage reference. This specification assumes ideal conditions, with no additional noise being fed into AVREFP/AVREFM lines.

In a customer-designed board, care should be taken to minimize ground loops and power supply line impedance to the Analog voltage reference pins. For the RSKRL78G14 board, connector J4 is the shortest, most convenient place to wire up the DAC and ADC lines on G14 MCU ports P2 and P15. DAC and ADC analog reference pins AVREFP and AVREFM are connected to VDD and VSS/Ground respectively, by connecting to connector J12.



**Figure 13: Standard RSKRL78G14 board (part #R0K50104PC000BE)**

In wiring diagram Figure 14, ANI11 ADC input is used for directly checking the DAC output errors (without DAC dithering), and ANI14 ADC input used for checking/correcting the DAC dithering Low-pass filtered output value.



**Figure 14: Recommended wiring for DAC dithering Sample SW project using RSKRL78G14 board**

### 11. Documents for Reference

User's Manual:  
 RL78/G14 User's Manual Manual: Hardware Rev.3.30 (R01UH0200EJ0330)  
 RL78 Family User's Manual: Software Rev.2.00 (R01US0015EJ0200)  
 (The latest versions of the documents are available on the Renesas Electronics Website.)

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# Revision History

Rev.	Date	Description	
		Page	Summary
1.00	10Aug2017		First edition

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